

Direct Determination of Crystal Structure

I. Monte Carlo Method

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(Received October 15, 1983)

Abstract

Electronic computer's program for direct determination of crystal structure by Monte Carlo Method is made for pyrenocine analyzed by Sato, Konomo, Sakumura, Furusaki, Matsumoto and Matsuzaki [Agri. Biol. Chem. 45, 795 (1981)]. The R-value for 316 strong reflections of the structure obtained from the structure with the smallest R-value among 61 structures which are obtained by using 52 reflections, becomes 0.27 by successive application of the method. The list of the program is shown.

1. Introduction

Direct determination of crystal structure has been discussed by many investigators in many respects. Although the author had been interested in the direct determination, he had no time to study sincerely the method. Recently, his paper concerning to criticism against space-groupoid theory was rejected by the editor of *Acta Crystallographica*. Taking this opportunity, he formed a resolution to study the direct determination.

For the beginning of the study, the author read the review of Furusaki (1982) on Monte Carlo method applying to phase-determination. According to him, the method of Vand (1960) applying Monte Carlo method to the direct determination has the following defects,

- (1) the probability hitting correct structure is too small,
- (2) the corrections in optimal shift method are too large,
- (3) there is no procedure correcting wrong structures.

The reason that the optimal shift method fails is very simple. If we suppose a very simple structure, Taylor series of the structure factor converges if $du_i = 2\pi dx_i$ is less than 1.0. Unless the series converges for large dx_i , we can not obtain the structure factor by successive approximation. The defects (1) and (3) can be avoided if we apply similar method with that of Metropolis (1953) in molecular dynamics.

Taking account of the recent development of electronic computer, the author judged

that crystal structures can be determined directly by Monte Carlo method. To compare with Furusaki's method, pyrenocine analyzed by Sato, Konomo, Sakumura, Furusaki, Matsumoto and Matsuzaki (1981), of which the coordinates of the atoms were informed by Furusaki (1983) was chosen as the testing material.

2. List of Program

The list of the program is shown at the last part of this paper. The program used at the 1st step of the calculation is as follows.

(1) The line 17 is deleted,

(2) the following line is inserted between the line 61 and 62,

IF(NTRY.GT.100) STOP

(3) the following lines are inserted between the line 66 and 67,

DO 70 I=1,NA

DO 80 J=1,3

CALL RANU2 (IX,RAN,1,ICON)

A=0.001*AINT(A)

GX(J,I)=HX(J,I)

80 CONTINUE

90 CONTINUE

(4) the following lines are inserted between the line 122 and 123.

IF(NCAL.GE.100.AND.RI.GE.0.2) GO TO 69

IF(NCAL.GE.300.AND.RI.GE.0.1) GO TO 69

3. Result

In our calculation, the structure factors calculated with the coordinates of pyrenocine were used instead of observed intensities. The scattering factors were substituted for the atomic numbers. Suitable starting structures were searched by using 52 reflections with $|F(h)| > 25.0$. After calculation of CPU time 1 hour by FACOM M382, we obtained 7 structures with $0.1 \leq R \leq 0.2$ and 1 structure with $R < 0.1$ among 61 structures. Finally we obtained the structure with $R = 0.27$ starting from the structure with the smallest R -value by successive application of our calculation. The results are summarized in the following list.

| | <i>initial R</i> | <i>final R</i> | <i>reflections</i> | $ F $ |
|-----------------|------------------|----------------|--------------------|-------|
| <i>1st step</i> | 0.728 | 0.063 | 52 | 25.0 |
| <i>2nd step</i> | 0.192 | 0.136 | 116 | 21.0 |
| <i>3rd step</i> | 0.227 | 0.215 | 196 | 18.0 |
| <i>4th step</i> | 0.285 | 0.271 | 316 | 15.0 |

4. Discussion

The change of the value of DX did not give any remarkable effect on the diminishing of R-value. The value DX is a constant and equal to 0.2 in the author's present program. The line 118 is to be revised to

IF (ARI.LE.0.001) GO TO 300

and the line 123 is to be deleted.

The convergence of *R*-value is very rapid. We can see the tendency of the convergence at very small number of NCAL. In our example, the value of RI at NCAL=100 is 0.0856, but the final NCAL is 1100 in the first step. The decreasing of *R*-value becomes small, when the number of the reflections becomes large. If the number of reflections increases, CPU time increases very much compared with diminishing of *R*-value. Our method is not profitable for the large number of reflections. The coordinates of atoms can be determined if the number of independent reflections is larger than 6NA, where NA is the number of independent atoms in a unit cell. It is better to limit the number of reflections within slightly larger than 6NA in the final step, and to refine the coordinates by the other method for larger reflections.

The author wished to improve his program to obtain structures with small *R*-value at once. The attempt failed almost all. The *R*-value could be diminished, but the increase of CPU time became very large. It is better to stop calculation and to examine another structure, if *R*-value is larger than the value previously determined at a given NCAL. This is valid for the case of the refinement.

There are three kinds of ways for improvement of our calculation,

- (A) to find more effective parameter than *R*-value,
- (B) to make slow the convergence of *R*-value,
- (C) to consider the set of reflections.

We can not find any parameter at present. There are two ways for the refinement concerning to (B). (1) The order of calculation between the line 125 and 185 is changed. This can be done by using random numbers. Although the result of the calculation by

the author did not show any effect, it should be effective for the refinement. (2) The calculation between the line 125 and 188 alternates between that by using LNR reflections and that by using LNR*c reflections with large rh , $rh = |E_o| - |E_c|/|E_o|$. In the author's example, R -value did not converge when $c=0.5$, and was improved considerably when $c=0.75$ and NCAL=10n-50n, but when NCAL=5n, R -value did not converge even though $c=0.75$. Even though (C) is not for the improvement of the program in the proper sense, it is very important for practical sense. We should choose lower order reflections in general.

Acknowledgement

The author thanks Mrs. K. Kawabata of Computer Center of our University for her kind help in this study.

References

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Sato, H., Konoma, K., Sakumura, S., Furusaki, A., Matsumoto, A., and Matsuzaki, T. (1981). Agric. Biol. Chem. **44**, 795-797.
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000001      DOUBLE PRECISION PAIT,SC,SF,H,F,HF,AF,DF,AH,AK,AL,SUMF,SUMHF,
000002      1B3,ARB,CC,HX,SX,AX,AY,AZ,CX,CY,CZ,GF,SUMDF,RIS
000003      DIMENSION SC(100),F(1000),HF(1000),AF(1000),GF(1000),
000004      1X(3,100),HX(3,100),SX(3,100),IH(3,1000),H(3,1000),DF(1000),
000005      2RAN(1),RIS(100)
000006      PAIT=6.283185307179586
000007      510 FORMAT(8I10)
000008      WRITE(6,650)
000009      WRITE(6,655)
000010      655 FORMAT(//,5X,'CPYSTAL      STRUCTURE DETERMINATION BY REDUCING',
000011      1 ' R-VALUE')
000012      C NR IS NUMBER OF TOTAL REFLECTIONS AND LNR IS NUMBER OF REFLECTIONS
000013      C USED IN THIS CALCULATION
000014      READ(5,510)NA,NR
000015      WRITE(6,611)NA,NR
000016      611 FORMAT(//,5X,'NUMBER      OF ATOMS =',I5,/
000017      15X,'NUMBER OF REFLECTIONS =',I5)
000018      WRITE(6,650)
000019      550 FORMAT(//,5X,'COORDINATES OF ATOMS')
000020      READ(5,501)(SC(J),(X(I,J),I=1,3),J=1,NA)
000021      501 FORMAT(2(F5.0,3F10.0))
000022      WRITE(6,601)(SC(J),(X(I,J),I=1,3),J=1,NA)
000023      601 FORMAT(2(5X,4F10.5))
000024      READ(5,501)(SC(J),(HX(I,J),I=1,3),J=1,NA)
000025      READ(5,511)((IH(I,J),I=1,3),J=1,NR)
000026      511 FORMAT(3I5)
000027      DO 10 I=1,NR
000028      DO 20 J=1,3
000029      H(J,I)=PAIT*IH(J,I)
000030      20 CONTINUE
000031      10 CONTINUE
000032      DO 30 I=1,NR
000033      F(I)=0.0
000034      AH=H(1,I)
000035      AK=H(2,I)
000036      AL=H(3,I)
000037      AHK=0.5*(IH(1,I)+IH(2,I))
000038      ALO=0.5*IH(3,I)
000039      CHK=AHK-AINT(AHK)
000040      CLO=ALO-AINT(ALO)
000041      DO 40 J=1,NA
000042      AX=X(1,J)
000043      AY=X(2,J)
000044      AZ=X(3,J)
000045      IF(ABS(CHK).LT.0.001.AND.ABS(CLO).LT.0.001) GO TO 41
000046      IF(ABS(CHK).LT.0.001.AND.ABS(CLO).GE.0.001) GO TO 42
000047      IF(ABS(CHK).GE.0.001.AND.ABS(CLO).LT.0.001) GO TO 43
000048      IF(ABS(CHK).GE.0.001.AND.ABS(CLO).GE.0.001) GO TO 44
000049      41 CONTINUE
000050      F(I)=F(I)+SC(J)*DCOS(AH*AX)*DCOS(AK*AY)*DCOS(AL*AZ)
000051      GO TO 40
000052      42 CONTINUE
000053      F(I)=F(I)-SC(J)*DCOS(AH*AX)*DSIN(AK*AY)*DSIN(AL*AZ)
000054      GO TO 40
000055      43 CONTINUE
000056      F(I)=F(I)-SC(J)*DSIN(AH*AX)*DCOS(AK*AY)*DSIN(AL*AZ)
000057      GO TO 40
000058      44 CONTINUE

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000052      F(I)=F(I)-SC(J)*DSIN(AH*AX)*DSIN(AK*AY)*DCOS(AL*AZ)
000053 40 CONTINUE
000054      AF(I)=DABS(F(I))
000055 30 CONTINUE
000056      READ(5,510)IX
000057      WRITE(6,615)IX
000058 615 FORMAT(1,5X,'INITIAL IX =',I10)
000059      NTRY=0
000060 69 CONTINUE
000061      NTRY=NTRY+1
000062      WRITE(6,650)
000063      WRITE(6,613)NTRY
000064 513 FORMAT(1//,5X,'TRIAL NUMBER =',I5)
000065      WRITE(6,614)
000066 514 FORMAT(1//,5X,'INITIAL COORDINATES')
000067      WRITE(6,601)(SC(J),(HX(I,J),I=1,3),J=1,NA)
000068      DX=0.2
000069      LNR=NR
000070      SUMF=0.0
000071      DO 90 I=1,LNR
000072      SUMF=SUMF+AF(I)
000073 90 CONTINUE
000074      NCAL=0
000075      NSTEP=0
000076 129 CONTINUE
000077      NSTEP=NSTEP+1
000078      SUMHF=0.0
000079      DO 130 I=1,LNR
000080      AH=H(1,I)
000081      AK=H(2,I)
000082      AL=H(3,I)
000083      AHK=0.5*(IH(1,I)+IH(2,I))
000084      ALO=0.5*IH(3,I)
000085      CHK=AHK-AINT(AHK)
000086      CLO=ALO-AINT(ALO)
000087      HF(I)=0.0
000088      DO 140 J=1,NA
000089      AX=HX(1,J)
000090      AY=HX(2,J)
000091      AZ=HX(3,J)
000092      IF(ABS(CHK).LT.0.001.AND.ABS(CLO).LT.0.001) GO TO 141
000093      IF(ABS(CHK).LT.0.001.AND.ABS(CLO).GE.0.001) GO TO 142
000094      IF(ABS(CHK).GE.0.001.AND.ABS(CLO).LT.0.001) GO TO 143
000095      IF(ABS(CHK).GE.0.001.AND.ABS(CLO).GE.0.001) GO TO 144
000096 141 CONTINUE
000097      HF(I)=HF(I)+SC(J)*DCOS(AH*AX)*DCOS(AK*AY)*DCOS(AL*AZ)
000098      GO TO 140
000099 142 CONTINUE
000100      HF(I)=HF(I)-SC(J)*DCOS(AH*AX)*DSIN(AK*AY)*DSIN(AL*AZ)
000101      GO TO 140
000102 143 CONTINUE
000103      HF(I)=HF(I)-SC(J)*DSIN(AH*AX)*DCOS(AK*AY)*DSIN(AL*AZ)
000104      GO TO 140
000105 144 CONTINUE
000106      HF(I)=HF(I)-SC(J)*DSIN(AH*AX)*DSIN(AK*AY)*DCOS(AL*AZ)
000107 140 CONTINUE
000108      GF(I)=HF(I)
000109      BB=DABS(HF(I))

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000110      CC=DABS(AF(I)-BB)
000111      SUMHF=SUMHF+CC
000112      130 CONTINUE
000113          RI=SUMHF/SUMF
000114          NS=NSTEP-1
000115          RIS(NSTEP)=RI
000116          IF(NS.EQ.0) GO TO 150
000117          ARI=ABS(RI-RIS(NS))
000118          IF(ARI.LE.0.001)DX=0.1★DX
000119      150 CONTINUE
000120          WRITE(6,602)NCAL,RI
000121          602 FORMAT(5X,I6,F10.5)
000122          WRITE(6,601)(SC(J),(HX(I,J),I=1,3),J=1,NA)
000123          IF(DX.LT.0.001) GO TO 300
000124      179 CONTINUE
000125          DO 200 I=1,NA
000126              SF=SC(I)
000127              DO 210 J=1,3
000128                  AX=HX(1,I)
000129                  AY=HX(2,I)
000130                  AZ=HX(3,I)
000131                  SX(1,I)=AX
000132                  SX(2,I)=AY
000133                  SX(3,I)=AZ
000134          CALL RANU2(IX,RAN,1,ICON)
000135          DO 220 II=1,5
000136          DO 230 JJ=1,2
000137          ADX=DX*II*(-1)**JJ
000138          ADX=ADX*RAN(1)
000139          SUMDF=0.0
000140          DO 240 K=1,LNR
000141              AHK=0.5*(IH(1,K)+IH(2,K))
000142              ALO=0.5*IH(3,K)
000143              CHK=AHK-AINT(AHK)
000144              CLO=ALO-AINT(ALO)
000145              AH=H(1,K)
000146              AK=H(2,K)
000147              AL=H(3,K)
000148              SX(J,I)=HX(J,I)+ADX
000149              CX=SX(1,I)
000150              CY=SX(2,I)
000151              CZ=SX(3,I)
000152              IF(ABS(CHK).LT.0.001.AND.ABS(CLO).LT.0.001) GO TO 251
000153              IF(ABS(CHK).LT.0.001.AND.ABS(CLO).GE.0.001) GO TO 252
000154              IF(ABS(CHK).GE.0.001.AND.ABS(CLO).LT.0.001) GO TO 253
000155              IF(ABS(CHK).GE.0.001.AND.ABS(CLO).GE.0.001) GO TO 254
000156      251 CONTINUE
000157          DF(K)=HF(K)+SF*(DCOS(AH*CX)*DCOS(AK*CY)*DCOS(AL*CZ)
000158          1-DCOS(AH*AX)*DCOS(AK*AY)*DCOS(AL*AZ))
000159          GO TO 255
000160      252 CONTINUE
000161          DF(K)=HF(K)-SF*(DCOS(AH*CX)*DSIN(AK*CY)*DSIN(AL*CZ)
000162          1-DCOS(AH*AX)*DSIN(AK*AY)*DSIN(AL*AZ))
000163          GO TO 255
000164      253 CONTINUE
000165          DF(K)=HF(K)-SF*(DSIN(AH*CX)*DCOS(AK*CY)*DSIN(AL*CZ)
000166          1-DSIN(AH*AX)*DCOS(AK*AY)*DSIN(AL*AZ))
000167          GO TO 255

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000165 254 CONTINUE
000166    DF(K)=HF(K)-SF*(DSIN(AH*CX)*DSIN(AK*CY)*DCOS(AL*CZ)
000167      1-DSIN(AH*AX)*DSIN(AK*AY)*DCOS(AL*AZ))
000168 255 CONTINUE
000169    BB=AF(K)-DABS(DF(K))
000170    ABB=DABS(BB)
000171    SUMDF=SUMDF+ABB
000172 240 CONTINUE
000173    IF(SUMDF.GE.SUMHF) GO TO 230
000174    SUMHF=SUMDF
000175    HX(J,I)=SX(J,I)
000176    DO 260 K=1,LNR
000177    GF(K)=DF(K)
000178 260 CONTINUE
000179 230 CONTINUE
000180 220 CONTINUE
000181    HX(J,I)=HX(J,I)-DINT(HX(J,I))
000182    DO 270 K=1,LNR
000183    HF(K)=GF(K)
000184 270 CONTINUE
000185 210 CONTINUE
000186 200 CONTINUE
000187    NCAL=NCAL+1
000188    IF(MOD(NCAL,100).EQ.0) GO TO 129
000189    GO TO 179
000190 300 CONTINUE
000191    WRITE(6,660)
000192    660 FORMAT(1H1)
000193    WRITE(6,618)RI
000194    618 FORMAT(/,5X,'R =',F10.5)
000195    WRITE(6,656)NCAL
000196    656 FORMAT(/,5X,'NCAL =',I6)
000197    WRITE(6,652)
000198    652 FORMAT(/,5X,'HX(I),I=1,3,J=1,NA')
000199    WRITE(6,601)(SC(J),(HX(I,J),I=1,3),J=1,NA)
000200    WRITE(6,653)
000201    653 FORMAT(///,5X,'COMPARISON BETWEEN FI AND HF')
000202    WRITE(6,654)
000203    654 FORMAT(/,5X,' H   K   L       F       HF')
000204    LNRT=LNR/2
000205    DO 450 I=1,LNRT
000206    II=I+LNRT
000207    WRITE(6,603)IH(1,I),IH(2,I),IH(3,I),F(I),HF(I),
000208      1IH(1,II),IH(2,II),IH(3,II),F(II),HF(II)
000209    603 FORMAT(2(5X,3I5,5X,2F10.5))
000210 450 CONTINUE
000211    STOP
000212    END

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R = 0.27088

NCAL = 600

HX(I), I=1,3, J=1,NA)

| | | | | | | | |
|---------|----------|----------|----------|---------|----------|----------|----------|
| 6.00000 | 0.71199 | -0.05934 | 0.91037 | 6.00000 | 0.09783 | -0.53986 | -0.40909 |
| 6.00000 | -0.96971 | 0.09443 | 0.35812 | 6.00000 | 0.14873 | 0.58056 | 0.15406 |
| 6.00000 | 0.91594 | 0.38379 | 0.89969 | 8.00000 | 0.59930 | 0.13469 | 0.41039 |
| 8.00000 | 0.47160 | 0.56049 | 0.27381 | 8.00000 | -0.73496 | 0.13723 | 0.63480 |
| 6.00000 | 0.97417 | 0.42753 | -0.22885 | 6.00000 | -0.02819 | -0.94201 | 0.22782 |
| 6.00000 | -0.41274 | 0.86091 | 0.99299 | 6.00000 | 0.71696 | 0.49314 | -0.13170 |
| 6.00000 | 0.02786 | -0.05943 | -0.22846 | 6.00000 | 0.53330 | -0.85232 | 0.53986 |
| 8.00000 | -0.20732 | 0.76515 | -0.01257 | | | | |

COMPARISON BETWEEN FI AND HF

| H | K | L | F | HF | 7 | 10 | 14 | -17.78585 | -17.80076 |
|---|----|----|-----------|-----------|---|----|----|-----------|-----------|
| 0 | 0 | 6 | -25.09268 | -14.95579 | 7 | 11 | 12 | 18.42698 | -2.08140 |
| 0 | 0 | 8 | 25.67503 | 36.30489 | 8 | 1 | 4 | 36.52656 | -36.15403 |
| 0 | 0 | 14 | 21.11401 | 24.93284 | 8 | 1 | 8 | 19.85971 | 2.87210 |
| 0 | 2 | 0 | 33.31723 | 27.29699 | 8 | 1 | 10 | -29.74365 | 32.80463 |
| 0 | 2 | 1 | 30.88285 | -31.58985 | 8 | 1 | 11 | -33.80591 | -34.02596 |
| 0 | 2 | 2 | -25.18615 | -26.02203 | 8 | 1 | 12 | 39.28876 | -46.17853 |
| 0 | 2 | 7 | -26.85451 | 24.88287 | 8 | 1 | 14 | -18.45007 | 3.98707 |
| 0 | 2 | 13 | 16.98445 | -22.49849 | 8 | 3 | 3 | -19.56784 | -27.68298 |
| 0 | 4 | 0 | -26.12035 | -21.76359 | 8 | 3 | 5 | 22.02006 | 21.6073 |
| 0 | 4 | 1 | 38.20701 | -41.88622 | 8 | 3 | 6 | -16.81631 | 2.72721 |
| 0 | 4 | 2 | -16.43562 | -4.03786 | 8 | 3 | 10 | -26.96322 | 22.53408 |
| 0 | 4 | 3 | -22.56163 | 6.87509 | 8 | 3 | 11 | -60.35148 | -59.67865 |
| 0 | 4 | 7 | -20.80638 | 20.32627 | 8 | 3 | 13 | 18.63689 | 18.63249 |
| 0 | 4 | 9 | 15.78675 | -9.28975 | 8 | 5 | 4 | -22.91858 | 16.02275 |
| 0 | 6 | 0 | -17.60010 | -21.55054 | 8 | 5 | 5 | 28.59382 | 27.08275 |
| 0 | 6 | 1 | 25.27786 | -22.48151 | 8 | 5 | 9 | 27.72992 | 32.30419 |
| 0 | 6 | 2 | 21.13388 | 19.12739 | 8 | 5 | 11 | -15.07119 | -9.64434 |
| 0 | 6 | 5 | 19.66276 | -12.82512 | 8 | 5 | 12 | -23.10377 | 23.96374 |
| 0 | 6 | 6 | 17.54599 | 5.37118 | 8 | 5 | 13 | 32.46067 | 36.68259 |
| 0 | 6 | 10 | 17.25061 | 1.25790 | 8 | 7 | 9 | 17.66455 | 9.75103 |
| 0 | 8 | 2 | 24.57188 | 37.57106 | 8 | 7 | 10 | 30.07034 | -30.11983 |
| 0 | 8 | 4 | -23.22448 | -22.65559 | 8 | 7 | 12 | -19.23164 | 20.89339 |
| 0 | 8 | 6 | 27.65312 | 23.87571 | 8 | 7 | 14 | 32.79320 | -33.96154 |
| 0 | 8 | 12 | -17.74308 | -4.03701 | 8 | 9 | 1 | -15.42204 | -8.82307 |
| 0 | 10 | 3 | 21.03520 | -24.71901 | 8 | 9 | 6 | 17.90573 | -17.90585 |
| 0 | 10 | 4 | -26.90871 | -26.95470 | 8 | 9 | 8 | -19.24109 | 26.83257 |
| 0 | 12 | 3 | 23.58600 | -23.62130 | 8 | 9 | 12 | -17.06271 | 20.75206 |
| 0 | 12 | 5 | -29.04481 | 31.19637 | 8 | 9 | 13 | -28.57053 | -29.47929 |
| 0 | 12 | 10 | -23.94357 | -25.25570 | 8 | 9 | 14 | 17.86016 | -17.92654 |
| 0 | 12 | 12 | -18.48149 | -12.53172 | 8 | 11 | 6 | 16.40082 | -25.51929 |
| 0 | 14 | 0 | 25.06842 | 37.69684 | 8 | 11 | 11 | 21.22989 | 19.30361 |
| 0 | 14 | 3 | -15.03015 | -6.17394 | 8 | 13 | 1 | 17.01951 | 17.01826 |
| 0 | 14 | 4 | 17.48867 | 9.14095 | 8 | 13 | 8 | 19.77828 | -11.98213 |
| 0 | 14 | 5 | -29.79658 | 32.20839 | 8 | 13 | 14 | -18.02881 | 22.77450 |
| 0 | 14 | 8 | 23.30136 | 15.56136 | 8 | 1 | 4 | 16.00588 | 4.60941 |
| 0 | 14 | 13 | -15.98586 | 16.17413 | 8 | 1 | 5 | 15.47387 | 7.68795 |
| 1 | 0 | 2 | -20.37270 | -32.85221 | 8 | 1 | 10 | 18.91880 | -14.02246 |
| 1 | 0 | 6 | 18.36893 | 18.42010 | 8 | 2 | 9 | -15.66012 | 29.89783 |
| 1 | 1 | 8 | -15.52188 | 7.90685 | 8 | 3 | 5 | 19.45185 | 12.74663 |
| 1 | 2 | 1 | 21.33176 | -13.33262 | 8 | 3 | 8 | -15.14765 | 10.32101 |
| 1 | 4 | 2 | 16.63607 | 6.53905 | 8 | 3 | 9 | -18.06576 | -10.96841 |
| 1 | 5 | 2 | 15.43821 | -2.30137 | 8 | 4 | 6 | -15.31431 | -1.68612 |
| 1 | 7 | 0 | -19.90821 | -28.54316 | 8 | 5 | 7 | -16.41087 | -9.94095 |
| 1 | 7 | 4 | 21.95279 | -14.42958 | | | | | |
| 1 | 7 | 5 | 15.29501 | -10.87221 | | | | | |

Direct Determination of Crystal Structure

| | | | | | | | | | |
|---|----|----|-----------|-----------|----|----|----|-----------|-----------|
| 1 | 8 | 3 | 23.18581 | -2.56528 | 9 | 5 | 14 | 16.54866 | 5.93180 |
| 1 | 10 | 12 | 16.18983 | 10.15781 | 9 | 7 | 13 | -19.52522 | 8.14740 |
| 1 | 12 | 5 | -17.22517 | 16.98199 | 9 | 7 | 14 | 16.90077 | -6.34037 |
| 1 | 13 | 3 | -20.43496 | -25.77362 | 9 | 9 | 8 | -15.75614 | 6.94399 |
| 1 | 14 | 11 | -16.08753 | 17.88961 | 9 | 10 | 14 | -22.37058 | -30.84423 |
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